## POWER ELECTRONICS AND PLC

# [TH-5]

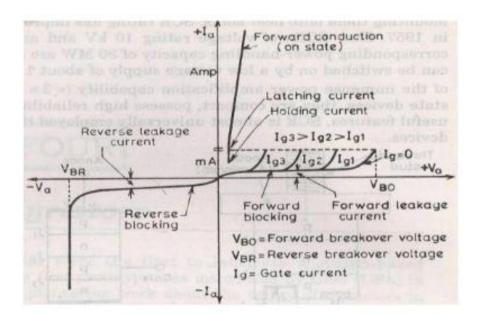
# 5<sup>TH</sup> SEM ELECTRICAL ENGG.

Under SCTE&VT, Odisha

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V<sub>BO</sub>=Forward breakover voltage

 $V_{BR}$ =Reverse breakover voltage

 $I_a$ =Gate current

 $V_a$ =Anode voltage across the thyristor terminal A,K.

 $I_a$ =Anode current

It can be inferred from the static V-I characteristic of SCR. SCR have 3 modes of operation:

- Reverse blocking mode
- 2. Forward blocking mode ( off state)
- Forward conduction mode (on state)

#### 1. Reverse Blocking Mode

When cathode of the thyristor is made positive with respect to anode with switch open thyristor is reverse biased. Junctions  $J_1$  and  $J_2$  are reverse biased where junction  $J_2$  is forward biased. The device behaves as if two diodes are connected in series with reverse voltage applied across them.

- A small leakage current of the order of few mA only flows. As the thyristor is reverse biased and in blocking mode. It is called as acting in reverse blocking mode of operation.
- Now if the reverse voltage is increased, at a critical breakdown level called reverse breakdown voltage V<sub>BR</sub>, an avalanche occurs at J<sub>1</sub> and J<sub>3</sub> and the reverse

current increases rapidly. As a large current associated with  $V_{BR}$  and hence more losses to the SCR.

This results in Thyristor damage as junction temperature may exceed its maximum temperature rise.

#### 2. Forward Blocking Mode

When anode is positive with respect to cathode, with gate circuit open, thyristor is said to be forward biased.

Thus junction  $J_1$  and  $J_3$  are forward biased and  $J_2$  is reverse biased. As the forward voltage is increases junction  $J_2$  will have an avalanche breakdown at a voltage called forward breakover voltage  $V_{BO}$ . When forward voltage is less then  $V_{BO}$  thyristor offers high impedance. Thus a thyristor acts as an open switch in forward blocking mode.

#### 3. Forward Conduction Mode

Here thyristor conducts current from anode to cathode with a very small voltage drop across it. So a thyristor can be brought from forward blocking mode to forward conducting mode:

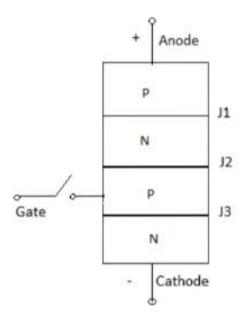
- By exceeding the forward breakover voltage.
- 2. By applying a gate pulse between gate and cathode.

During forward conduction mode of operation thyristor is in on state and behave like a close switch. Voltage drop is of the order of 1 to 2mV. This small voltage drop is due to ohmic drop across the four layers of the device.

### Different turn ON methods for SCR

- Forward voltage triggering
- Gate triggering
- 3.  $\frac{dv}{dt}$  triggering
- 4. Light triggering
- 5. Temperature triggering

#### 1. Forward voltage triggering



A forward voltage is applied between anode and cathode with gate circuit open.

- Junction J<sub>1</sub> and J<sub>3</sub> is forward biased.
- Juntion J<sub>2</sub> is reverse biased.
- As the anode to cathode voltage is increased breakdown of the reverse biased junction *J*<sub>2</sub> occurs. This is known as avalanche breakdown and the voltage at which this phenomena occurs is called forward breakover voltage.
- The conduction of current continues even if the anode cathode voltage reduces below
   V<sub>BO</sub> till I<sub>a</sub> will not go below I<sub>h</sub>. Where I<sub>h</sub> is the holding current for the thyristor.

#### 2. Gate triggering

This is the simplest, reliable and efficient method of firing the forward biased SCRs. First SCR is forward biased. Then a positive gate voltage is applied between gate and cathode. In practice the transition from OFF state to ON state by exceeding  $V_{BO}$  is never employed as it may destroy the device. The magnitude of  $V_{BO}$ , so forward breakover voltage is taken as final voltage rating of the device during the design of SCR application.

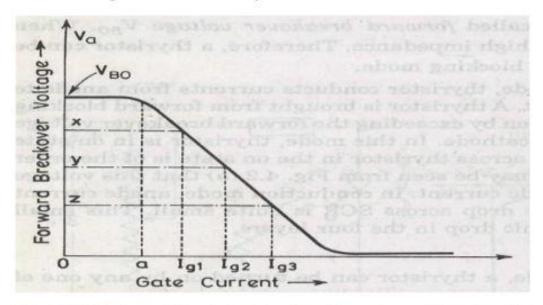
First step is to choose a thyristor with forward breakover voltage (say 800V) higher than the normal working voltage. The benefit is that the thyristor will be in blocking state with normal working voltage applied across the anode and cathode with gate open. When we require the turning ON of a SCR a positive gate voltage between gate and cathode is applied. The point to be noted that cathode n-layer is heavily doped as compared to gate p-layer. So when gate supply is given between gate and cathode gate p-layer is flooded with electron from cathode n-layer. Now the thyristor is forward biased, so some of these electron reach junction  $J_2$ . As a result width of  $J_2$  breaks down or conduction at  $J_2$  occur at a voltage less than  $V_{BO}$ . As  $I_g$  increases  $V_{BO}$  reduces which decreases then turn ON time. Another important point is duration for which the gate current is applied should be more then turn ON time. This means

that if the gate current is reduced to zero before the anode current reaches a minimum value known as holding current, SCR can't turn ON.

In this process power loss is less and also low applied voltage is required for triggering.

#### 3. dv/dt triggering

This is a turning ON method but it may lead to destruction of SCR and so it must be avoided.



When SCR is forward biased, junction  $J_1$  and  $J_3$  are forward biased and junction  $J_2$  is reversed biased so it behaves as if an insulator is place between two conducting plate. Here  $J_1$  and  $J_3$  acts as a conducting plate and  $J_2$  acts as an insulator.  $J_2$  is known as junction capacitor. So if we increase the rate of change of forward voltage instead of increasing the magnitude of voltage. Junction  $J_2$  breaks and starts conducting. A high value of changing current may damage the SCR. So SCR may be protected from high  $\frac{dv}{dt}$ .

$$q = cv$$

$$I_a = c \frac{dv}{dt}$$

$$I_a \alpha \frac{dv}{dt}$$

#### 4. Temperature triggering

During forward biased,  $J_2$  is reverse biased so a leakage forward current always associated with SCR. Now as we know the leakage current is temperature dependant, so if we increase the temperature the leakage current will also increase and heat dissipitation of junction  $J_2$  occurs. When this heat reaches a sufficient value  $J_2$  will break and conduction starts.

Disadvantages

### Rise time $(t_r)$

Time during which

- Anode current rises from 0.1 I<sub>a</sub> to 0.9 I<sub>a</sub>
- Forward blocking voltage falls from 0.9V<sub>a</sub> to 0.1V<sub>a</sub>. V<sub>a</sub> is the initial forward blocking voltage.

### Spread time $(t_p)$

- Time taken by the anode current to rise from 0.9I<sub>a</sub> toI<sub>a</sub>.
- 2. Time for the forward voltage to fall from 0.1Vo to on state voltage drop of 1 to 1.5V. During turn on, SCR is considered to be a charge controlled device. A certain amount of charge is injected in the gate region to begin conduction. So higher the magnitude of gate current it requires less time to inject the charges. Thus turn on time is reduced by using large magnitude of gate current.

## How the distribution of charge occurs?

As the gate current begins to flow from gate to cathode with the application of gate signal. Gate current has a non uniform distribution of current density over the cathode surface. Distribution of current density is much higher near the gate. The density decrease as the distance from the gate increases. So anode current flows in a narrow region near gate where gate current densities are highest. From the beginning of rise time the anode current starts spreading itself. The anode current spread at a rate of 0.1mm/sec. The spreading anode current requires some time if the rise time is not sufficient then the anode current cannot spread over the entire region of cathode. Now a large anode current is applied and also a large anode current flowing through the SCR. As a result turn on losses is high. As these losses occur over a small conducting region so local hot spots may form and it may damage the device.

# Switching Characteristics During Turn Off

Thyristor turn off means it changed from ON to OFF state. Once thyristor is oON there is no role of gate. As we know thyristor can be made turn OFF by reducing the anode current below the latching current. Here we assume the latching current to be zero ampere. If a forward voltage is applied across the SCR at the moment it reaches zero then SCR will not be able to block this forward voltage. Because the charges trapped in the 4-layer are still favourable for conduction and it may turn on the device. So to avoid such a case, SCR is reverse biased for some time even if the anode current has reached to zero.

So now the turn off time can be different as the instant anode current becomes zero to the instant when SCR regains its forward blocking capability.

$$t_q = t_{rr} + t_{qr}$$

Where,